## Problem 10.31

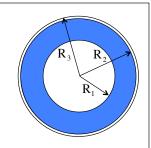
A tire can be modeled as three pieces, two side-walls and one tread pad.

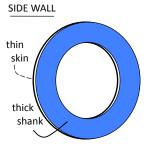
The side-wall: If you took a pair of heavy duty scissors and cut one of the side-walls away from the rest of the tire, you would end up with a very thin skinned, thick shanked cylinder (see sketch).

Although I always like to derive my expressions (something you should be able to do for a cylinder), the text's Solution Manual seems to think that you can start with the moment of inertia of a cylinder as a given quantity. That expression is:

$$I_{cyl} = \frac{1}{2} m_{cyl} \left( R_1^2 + R_2^2 \right)$$

where  $R_1$  is the inside radius and  $R_2$  is the outside radii not of the tire but, rather, the outside radius of the cut swath.





thin

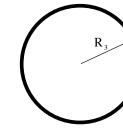
skin

thick

shank

1.)

As for the relatively THIN tread pad, because it is so thin it is tempting to assume that all of the mass is located a distance  $R_2$  meters from the center and go from there. In that scenario, and remember what the moment of inertia asks us to do, we would go out from the axis in question until we found our mass at the assumed position  $R_3$ , then multiply that mass by the square of that distance. This would lead to a *moment of inertia* of the tread pad of:

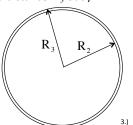


$$I_{\text{treadPad}} = m_{\text{pad}} R_3^2$$

(Why? Because all of the mass would be assumed to be a distance  $R_3$  out.)

The problem with this is that in reality, the pad is also a cylinder with an inside and outside radius. In other words, the moment of inertia for it should also be of the form:

 $I_{pad} = \frac{1}{2} \left[ \rho \left( \pi \left( R_3^4 - R_2^4 \right) t_{pad} \right) \right]$ 



where the "r" values are defined on the sketch.

We are given the volume mass density of the rubber (o), so knowing the volume of the side-wall, we can determine its mass. Noting that volume is *surface* area times thickness "t", where the surface area is

$$\pi R_{2}^{2} - \pi R_{1}^{2}$$

we can write the mass as:

$$m_{\text{sideWall}} = \rho \left( \left( \pi R_2^2 - \pi R_1^2 \right) t_{\text{wall}} \right)$$

With two side-walls, the net moment of inertia due to both will be (note that the last line is a simplification of the R terms done to save space):

$$\begin{split} I_{2\text{sideWalls}} &= 2 \bigg[ \frac{1}{2} \qquad m_{\text{sideWall}} \qquad \left( R_{1}^{2} + R_{2}^{2} \right) \bigg] \\ &= 2 \bigg[ \frac{1}{2} \bigg[ \rho \big( \left( \pi R_{2}^{2} - \pi R_{1}^{2} \right) t_{\text{wall}} \big) \bigg] \big( R_{1}^{2} + R_{2}^{2} \big) \bigg] \\ &= 2 \bigg[ \frac{1}{2} \bigg[ \rho \big( \pi \big( R_{2}^{4} - R_{1}^{4} \big) t_{\text{wall}} \big) \bigg] \bigg] \end{split}$$

Using that while omitting units and sig figs to conserve space, the total moment of inertia for the entire structure then becomes:

$$\begin{split} I = & \sqrt{\left[\frac{1}{2}\left[\rho\left(\pi\left(R_{2}^{4} - R_{1}^{4}\right)t_{wall}\right)\right]\right]} + \left[\frac{1}{2}\left[\rho\left(\pi\left(R_{3}^{4} - R_{2}^{4}\right)t_{pad}\right)\right]\right]} \\ = & \left[\left[\left(1.1x10^{3}\right)\pi\left((.305)^{4} - (.165)^{4}\right)(6.35x10^{-3})\right]\right] \\ & + \left[\frac{1}{2}\left[\left(1.1x10^{3}\right)\pi\left((.33)^{4} - (.305)^{4}\right)(.2)\right]\right] \\ = & \left[\left(1.1x10^{3}\right)\pi\right]\left(\left[\left((.305)^{4} - (.165)^{4}\right)(6.35x10^{-3})\right] + \left[\frac{1}{2}\left[\left((.33)^{4} - (.305)^{4}\right)(.2)\right]\right]\right) \\ = & 1.28 \text{ kg} \cdot \text{m}^{2} \end{split}$$

The moral of the story? When trying to determine the moment of inertia of a system that has many pieces to it, determine the moment of inertia due to EACH piece, then add them all together.

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